

Art Unit:
Serial No:

To be Assigned
U.S. National Phase of PCT/EP00/02839

matter being deleted from the specification of record. The Substitute Specification does not include new matter.

In addition, by the present amendment, claims 1-27 have been amended to conform to U.S. Practice and to correct other informalities. These amendments are not considered to narrow the scope of the claims.

The Applicants respectfully submit that no new matter has been added by this Preliminary Amendment, and respectfully requests entry of this preliminary amendment.

CONCLUSION

In view of the foregoing amendments and remarks, the Applicants respectfully submit that the pending claims in the above-identified application are in condition for allowance, and a notice to that effect is earnestly solicited.

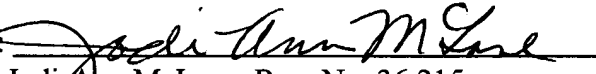
If the present application is found by the Examiner not to be in condition for allowance, the Applicants hereby request a telephone or personal interview to facilitate the resolution of any remaining matters. Applicants' attorney may be contacted by telephone at the number indicated below to schedule such an interview.

Art Unit:
Serial No:

To be Assigned
U.S. National Phase of PCT/EP00/02839

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Version with marking to show changes to claims

1. (Amended Once) A steering device for vehicles[, comprising;] including a steering shaft,
the steering device comprising:

[a steering shaft [(20)], a sensor [(35)] for determining the movement of said steering shaft, and a circuit [(40)] for evaluating the measuring signals of the sensor [(35)], [characterised in that];

coded microstructures [(31)] are provided on the steering shaft [(20)] and/or on a device that is connected to the steering shaft in a non-positive manner, that a sensor [(35)] is provided, which detects the microstructures [(31)] and outputs associated measuring signals, and that an electronic circuit [(40)] is provided, to which the measuring signals of the sensor [(35)] are fed and which outputs electronic signals for steering.

2. [A] The steering device [according to] of claim 1, [characterised in that] wherein the microstructures [(31)] form a succession of sequences arranged in an axial direction on the steering shaft [(20)] and/or the device non-positively connected thereto.

3. [A] The steering device [according to] of claim 2, [characterised in that] wherein each sequence comprises multiple and/or single structures arranged spatially in an azimuthal and/or axial direction and containing individual or block-type coding.

4. [A] The steering device [according to] of claim 2 [or 3], [characterised in that] wherein the sequences contain bit coding.

Art Unit:
Serial No:

To be Assigned
U.S. National Phase of PCT/EP00/02839

5. [A] The steering device [according to any] of claim[s] 2 [to 4], [characterised in that] wherein a plurality of sequences are combined in a block, the blocks being distinguishable from each other by coding.

6. [A] The steering device [according to any] of claim[s] 2 [to 5], [characterised in that] wherein the sequences arranged in an axial direction are present in redundant form, offset parallel more than once over the periphery of the steering shaft [(20)] and/or device.

7. [A] The steering device [according to any] of [the preceding] claim[s] 1, [characterised in that] wherein the microstructures [(31)] are in complementary form.

8. [A] The steering device [according to any] of [the preceding] claim[s] 1, [characterised in that] wherein the smallest details of the microstructures [(31)] have lateral dimensions of 5 nm to 5 mm.

9. [A] The steering device [according to] of claim 8, [characterised in that] wherein the smallest details of the microstructures [(31)] have lateral dimensions of 1 μ m to 1 mm.

10. [A] The steering device [according to] of [any of the preceding] claim[s] 1, [characterised in that] wherein the microstructures [(31)] have a thickness of 5 nm to 1 mm.

11. [A] The steering device [according to] of claim 10, [characterised in that] wherein the microstructures [(31)] have a thickness of 100 nm to 100 μ m.

Art Unit:
Serial No:

To be Assigned
U.S. National Phase of PCT/EP00/02839

12. [A] The steering device [according to any] of [the preceding] claim[s] 1, [characterised in that] wherein the microstructures [(31)] have a level surface and are levelled by a [planarising] planarizing method.

13. [A] The steering device [according to any] of [the preceding] claim[s] 1, [characterised in that] wherein the microstructures are built up from or covered with tribological hard-material layered systems.

14. [A] The steering device [according to] of claim 13, [characterised in that] wherein the hard-material layered systems are single films or multi-layer films of TiN and/or TiAlN and/or TiCN films and/or aluminium oxide films and/or amorphous diamantine hydrocarbon films with and without metal doping and/or amorphous CN films and/or cubic boron nitride films and/or diamond films.

15. [A] The steering device [according to any] of [the preceding] claim[s] 1, [characterised in that] wherein the sensors [(35)] are arranged in the form of a line and/or array.

16. [A] The steering device [according to any] of [the preceding] claim[s] 1, [characterised in that] wherein the sensors [(35)] are optical sensors.

17. [A] The steering device [according to] of claim 16, [characterised in that] wherein the sensors [(35)] are optical fibreglass sensors.

18. [A] The steering device [according to] of claim 17, [characterised in that] wherein the sensors [(35)] are fibre-optical double or multiple sensors.

Art Unit:
Serial No:

To be Assigned
U.S. National Phase of PCT/EP00/02839

19. [A] The steering device [according to any] of claim[s] 16 [to 18], [characterised in that] wherein the microstructures are in the form of a reflection hologram.

20. [A] The steering device [according to any] of claim[s] 1 [to 15], [characterised in that] wherein the sensors [(35)] are magnetic sensors.

21. [A] The steering device [according to] of claim 20, [characterised in that] wherein the magnetic sensors are in a linear arrangement for reading a multi-bit code, particularly an 8-bit code.

22. [A] The steering device [according to] of claim 20 [or 21], [characterised in that] wherein the sensor [(35)] has a reading head with polar structures arranged on an arc matching the diameter of the steering shaft [(20)].

23. A method of making a steering device [according to any of the preceding claims, characterised in that the] including a steering shaft, the method comprising the steps of:

applying coded microstructures on the steering shaft [(20)] or on [the] a device non-positively connected to the shaft [are produced] using thin film methods, and that structuring is effected by photo-lithographic methods[.];

detecting the microstructures and outputting an associated measuring signal; and
evaluating the measuring signal to determine appropriate action for steering control.

24. [A] The method [according to] of claim 23, [characterised in that] wherein the thin-film method is a PVD and/or CVD method.

Art Unit:
Serial No:

To be Assigned
U.S. National Phase of PCT/EP00/02839

25. [A] The method [according to] of claim 23 [or 24], [characterised in that] wherein the microstructures are formed by a dry etching process and/or a wet-chemical etching process.

26. [A] The method [of making a steering device according to any] of claim[s 1 to 22] 23, [characterised in that] wherein the microstructures are produced by a laser beam process.

27. [A] The method [according to] of claim 26, [characterised in that] wherein the laser beam process used is a direct-writing laser ablation process and/or a laser-lithographic process and/or a direct-action mask-related laser-structuring process.

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Comparison Copy
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JC09 Rec'd PCT/PTO 28 SEP 2001

1 NH1366-B

2
3 Steering device for vehicles STEERING DEVICE FOR VEHICLES

4
5
6 BACKGROUND

7 1. The invention relates to a steering device for vehicles, comprising a
8 steering shaft, a sensor for determining the movement of said steering
9 shaft, and a circuit for evaluating the measuring signals of the
10 sensor. Technical Field

11
12 The present application is directed to a steering device for vehicles, and in
13 particular to a steering device comprising a steering shaft, a sensor for determining
14 the movement of the steering shaft, and a circuit for evaluating the measuring
15 signals of the sensor.

16
17 2. Background of Related Art

18 Vehicle steering mechanisms may take different forms. Rack steering is
19 used particularly often. A driver exerts a torque on a steering column via a steering
20 wheel. Rack and pinion steering is used particularly often. With rack steering,
21 a driver exerts a torque on a steering column via a steering wheel. Direct power
22 transmission then continues via a pinion, i.e. a gear wheel, to a rack. Longitudinal
23 movement of the rack is also longitudinal movement of a steering shaft in or on
24 which the rack is mounted. The steering shaft in turn moves the steering gear, with
25 the vehicle wheels arranged on it and steered in this manner.

26
27 To assist the direct power transmission by the driver it is further known, in
28 hydraulic power-assisted steering mechanisms, to provide a pressure chamber in
29 which runs a piston fixed to the steering shaft. Longitudinal movement of the rack
30 results in longitudinal movement of a steering shaft in, or on which, the rack is

1 mounted. The steering shaft in turn moves the steering gear, with the vehicle
2 wheels arranged on it, and is steered in this manner.

3
4 To assist the direct power transmission by the driver it is also known to use
5 hydraulic power-assisted steering mechanisms, in which a pressure chamber runs
6 a piston fixed to the steering shaft. By controlling the pressure in the chamber
7 filled with hydraulic oil the piston can be moved, thereby assisting the steering
8 gear in addition to the power transmission by the driver. Alternatively the pinion
9 drive may be assisted by an electric motor. Alternatively, the pinion drive may be
10 assisted by an electric motor.

11
12 In order to provide these various forms of assistance it is naturally
13 desirable to have a measuring signal available which correlates with the state of
14 the steerage. The signal could then take over appropriate control to boost the
15 steering, for power-assisted steering and similar purposes and also allow self-
16 regulating systems. The signal could then take over appropriate control to boost
17 the steering, for power-assisted steering and similar purposes, and could also allow
18 for self-regulating systems. Over and above the control of the servo mechanism,
19 allowance should also be made for boosting measures to optimise the steering and
20 attenuation action of motor vehicles or simultaneous control of all four wheels and
21 other intelligent steering systems.

22
23 Various proposals have already been made for obtaining a signal which
24 correlates with the state of the steerage.

25
26 Thus it is proposed in DE 40 29 764 A1 to arrange length measuring means
27 between the steering wheel and the front axle, responding to displacement of the
28 steering rack. Thus, it is proposed in DE 40 29 764 A1 to arrange length
29 measuring means between the steering wheel and the front axle, responding to
30 displacement of the steering rack. Inductive or ohmic devices are proposed for

1 these means. [A design with two magneto-resistive sensors is known from EP 0
2 410 583 B1. Here the magnetic coupling is changed on movement of the steering
3 shaft, thus enabling the position to be determined. However this involves changing
4 the geometry of the steering shaft and also providing it with a groove, which apart
5 from the expense gives it a certain susceptibility to trouble. EP 0 376 456 B1 also
6 operates with a magnet. It is arranged on the steering shaft and surrounded by an
7 induction coil. Here, the magnetic coupling is changed on movement of the
8 steering shaft, thus enabling the position to be determined. However, this involves
9 changing the geometry of the steering shaft and also providing it with a groove,
10 which apart from the expense, gives it a certain susceptibility to trouble. EP 0 376
11 456 B1 also operates with a magnet which is arranged on the steering shaft and
12 surrounded by an induction coil. A change in induction can be associated with a
13 change in displacement.

14
15 Steering angle sensors operating with magnetic field sensors, so-called
16 Hall sensors, are known from DE 197 03 903 A1 and DE 197 52 346 A1.

17
18 These known proposals have the drawback that measurement only allows
19 restricted accuracy. [Another problematic feature is that the measurements are
20 relative, so that measuring errors add up over time. The proposals are not therefore
21 practicable for use in intelligent steering systems.

22
23 The proposals are not, therefore, practicable for use in intelligent steering
24 systems.

1 It is known from DE 37 03 591 C2, in a rack steering mechanism at the
2 end of the steering column, to measure the rotary angle of the column by
3 appropriately acting on an induction coil or a piezo power-measuring cell.
4 However the end of the steering column also carries the power transmission to the
5 steering rack and is both structurally confined and unfavourable for measurements,
6 particularly as a great deal of malfunctioning may take place there. However, the
7 end of the steering column also carries the power transmission to the steering rack
8 and is both structurally confined and unfavourable for measurements, particularly
9 as a great deal of malfunctioning may take place there.

10

11 The problem of the invention is to propose a steering device in which it is
12 possible to pick up a signal correlating with the state of the steering mechanism
13 and more suitable for controlling intelligent steering systems of that type.

14

15 The problem is solved, in that coded microstructures are provided on the steering
16 shaft and/or on a device that is connected to the steering shaft in a non-positive
17 manner, that a sensor is provided, which detects the microstructures and outputs
18 associated measuring signals, and that an electronic circuit is provided, to which
19 the measuring signals of the sensor are fed and which outputs electronic signals
20 to control the steering.

21

22 There is, therefore, needed in the art a steering device in which it is
23 possible to pick up a signal correlating with the state of the steering mechanism
24 and more suitable for controlling intelligent steering systems of that type.

25

26

SUMMARY

27

28 The present invention is directed to a steering device which includes coded
29 microstructures which are provided on the steering shaft and/or on a device that
30 is connected to the steering shaft in a non-positive manner; a sensor which detects
the microstructures and outputs associated measuring signals; and an electronic

1 circuit to which the measuring signals of the sensor are fed, and which outputs
2 electronic signals to control the steering.

3
4 The invention proposes a steering device for vehicles which allows
5 absolute measurements of position. ~~The disadvantages of the state of the art no~~
6 ~~longer exist.~~ Therefore, the disadvantages associated with the state of the art no
7 ~~longer exist.~~ The steering device according to the invention is more accurate and
8 supplies reproducible measuring signals. Regulation and/or control of the
9 movement of the steering shaft becomes possible, particularly for intelligent
10 steering systems.

11
12 Advanced surface techniques with processes indicating the microstructure
13 are thus combined with a high-resolution sensor, i.e. a detection system, with an
14 appropriate electronic circuit. The term "microstructures" refers here to structures
15 with dimensions in the micrometer range.

16
17 The term "detect" refers particularly to processes where contact-free
18 recognition takes place, preferably optically or magnetically. ~~However other~~
19 ~~detection methods which read, sense, feel or otherwise recognise also come into~~
20 ~~consideration. However, other detection methods which read, sense, feel or~~
21 ~~otherwise recognise also come into consideration.~~

22
23 The invention allows absolute determination of the position of the steering
24 shaft in a rapid, high-resolution and reliable manner, with resolution in the low
25 micrometer range. Falsification or trouble from electromagnetic fields or in the
26 region of the steering mechanism either does not take place or is negligible.

27
28 The invention may be applied successfully in particular to advanced, so-
29 called intelligent steering systems.
30

1 It is possible to equip the actual steering shaft with microstructures. The
 2 disadvantage of doing so would be the difficulty of manipulating the whole shaft
 3 during the fitting process. ~~In order to avoid this, smaller, interchangeable elements~~
 4 ~~which can be non-positively connected to the steering shaft, e.g. in bar form, may~~
 5 ~~be appropriately equipped then inserted.~~ In order to avoid this, smaller,
 6 interchangeable elements which can be non-positively connected to the steering
 7 shaft, e.g. in bar form, may be appropriately equipped, then inserted.

8
 9 The microstructures are advantageously formed so that they contain suitable
 10 coding, allowing the position of the steering shaft to be determined absolutely.

11
 12 The microstructures are advantageously formed so that they contain
 13 suitable coding, allowing the position of the steering shaft to be determined
 14 accurately.

15
 16 The microstructures are preferably detected by optical scanning methods,
 17 particularly using elements from microsystem technology. Microsystem
 18 technology is understood here as the fields of microstructure technology, micro-
 19 optics and fibre optics. Microlenses with diameters down to about 10 μm and
 20 focal lengths of the same order of magnitude may be used. If glass or other fibres
 21 and very small diameters are used, the microlenses can be fixed directly on the end
 22 face of the fibres. The entire system may have Y branches and is integrated with
 23 individual modules to form a compact microsystem. The modules may if
 24 appropriate be spatially offset over the optical fibres - for example to allow
 25 optoelectronic components and the evaluating electronic means to be operated
 26 optimally within low-temperature ranges. The modules may, if appropriate, be
 27 spatially offset over the optical fibres - for example to allow optoelectronic
 28 components and the evaluating electronic means to be operated optimally within
 29 low-temperature ranges.

1 Tribologically suitable film systems are advantageously applied to the
 2 steering shaft or to a linear means connected thereto without play, described as a
 3 device or measuring device. This may be done by thin film processes which have
 4 proved successful in other industrial fields. Special microstructures are produced
 5 by high-resolution structuring and etching processes. The microstructures are
 6 constituted so that they can be read by the sensors.

7
 8 The optical contrast, i.e. the difference in reflectivity, of the
 9 microstructures to the steering shaft surface below them may for example be
 10 modified, so that the pattern can be optically recognised by means of miniaturised
 11 fibre optical systems. Another example is to make the microstructures in the form
 12 of a reflection hologram, with coding as in the previous example (segment-wise)
 13 and with reading effected by a suitable miniaturised optical system. The
 14 functional layer may be crystalline or amorphous and the hologram may be written
 15 in a phase or angle code. The hologram may function in one frequency range
 16 (monochromatic) or more than one (coloured), and the information may be written
 17 (to the hologram) by a digital or analog process.

18
 19 ~~Other physical methods may be employed instead of or as well as optical sensors~~
 20 ~~or optically detectable microstructures. Thus microstructures may also be formed~~
 21 ~~in magnetic films, e.g. CoSm or NdFeB.~~ Other physical methods may be
 22 employed instead of, or as well as, optical sensors or optically detectable
 23 microstructures. Thus, microstructures may also be formed in magnetic films, e.g.
 24 CoSm or NdFeB. The sensors could then in particular be magnetic sensors,
 25 otherwise used in data storage technology.

26
 27 Microstructures are produced on the steering shaft or on the device non-
 28 positively connected thereto in the form of incremental markings. Tribologically
 29 optimised layer systems are preferred, using high-resolution lithographic or laser

1 technology methods suitable for three-dimensional applications. The lithographic
2 methods considered are of the photo, electronic, X ray and/or ionic type.

3

4 Multiple-layer or composite structures may equally be employed.

5

6 The patterns formed are preferably dimensioned in micrometers. The
7 layer systems, combined with an appropriate sensory recognition system, enable
8 the current position to be determined absolutely, to an accuracy of only a few
9 micrometers.

10

11 In an advantageous embodiment of the invention two complementary,
12 parallel patterns are provided with suitable coding, e.g. bit coding. In one
13 embodiment the marking structure comprises strips which are optically
14 distinguishable by reflection, the strip patterns containing binary L/O coding.

15

16 In this way the displacement-measuring system, which may be fully
17 integrated into the steering mechanism, can recognise the current absolute position
18 of the steerage in every operating phase by means of the bit coding.

19

20 Various patterns are possible. For example a dual code, a Gray code or
21 even stepped codes known *per se* from relevant mathematical processes may be
22 used.

1
2 It is particularly preferable to use optical sensors, especially fibre-optical
3 double sensors, for scanning the markings and microstructures. Multiple sensors
4 are also possible, especially in array form.
5

6 In a preferred method the microstructures are produced by applying thin
7 film techniques. These techniques are advantageously PVD (physical vapour
8 deposition) and/or CVD (chemical vapour deposition). As already mentioned,
9 structuring is effected by lithographical processes.
10

11 The microstructures can also be formed by dry etching and/or wet chemical
12 etching.
13

14 ~~Alternatively they may be made by laser beam techniques, e.g. direct-writing laser~~
15 ~~ablation processes and/or laser-lithographic processes and/or direct-action, mask-~~
16 ~~related laser structuring methods.~~
17

18 Alternatively, they may be made by laser beam techniques, e.g. direct-
19 writing laser ablation processes and/or laser-lithographic processes and/or direct-
20 action, mask-related laser structuring methods.
21

22 The microstructures are preferably built up from tribological hard-material
23 layered systems. Single or multi-layer films may be used. They are preferably
24 made of titanium nitride (TiN) and/or titanium aluminium nitride (TiAlN) and/or
25 titanium carbonitride (TiCN) films and/or aluminium oxide films and/or
26 amorphous diamantine hydrocarbon films with or without metal doping and/or
27 amorphous diamantine carbon films with or without metal doping and/or
28 amorphous CN films and/or cubic boron nitride films and/or diamond films.
29

1 Embodiments of the invention are explained below with reference to the
2 accompanying drawings, in which:

3
4 Fig. 1 is a diagrammatic section through essential elements of an embodiment of
5 a steering device according to the invention;

6
7 Fig. 2 is an alternative embodiment to Fig.

8 BRIEF DESCRIPTION OF THE DRAWINGS

9 It should be understood that the drawings are provided for the purpose of
10 illustration only and are not intended to define the limits of the invention. The
11 foregoing and other objects and advantages of the embodiments described herein
12 will become apparent with reference to the following detailed description when
13 taken in conjunction with the accompanying drawings in which:

14
15 FIG. 1 is a diagrammatic section through elements of an embodiment of
16 a steering device according to the invention;

17
18
19 Fig. 2 is an alternative embodiment to Fig. FIG. 2 is an alternative
20 embodiment to FIG. 1;

21
22 Fig. 3 is a diagrammatic representation of a microsystem-type sensor system for
23 an embodiment of the steering device according to the invention;

24
25 Fig. 4 is a detailed representation of a member from Fig. 3;

26
27 Fig. 5 is a detailed representation of an alternative embodiment of that member
28 from Fig. 3;

29

1 ~~Fig. 6~~ is a detailed representation of another member from Fig. 3;

2

3 ~~Fig. 7~~ shows an example of a microstructure;

4

5 ~~Fig. 8~~ shows an alternative embodiment of Fig. 7;

6

7 ~~Fig. 9~~ shows another alternative embodiment of Fig. 7;

8

9 ~~Fig. 10~~ is a diagrammatic section through a microstructure;

10

11 ~~Fig. 11 shows the Fig.~~ FIG. 3 is a diagrammatic representation of a microsystem-
12 type sensor system for an embodiment of the steering device according to the
13 invention;

14

15 FIG. 4 is a detailed representation of a member from FIG. 3;

16

17 FIG. 5 is a detailed representation of an alternative embodiment of that
18 member from FIG. 3;

19

20 FIG. 6 is a detailed representation of another member from FIG. 3;

21

22 FIG. 7 shows an example of a microstructure;

23

24 FIG. 8 shows an alternative embodiment of FIG. 7;

25

26 FIG. 9 shows another alternative embodiment of FIG. 7;

27

28 FIG. 10 is a diagrammatic section through a microstructure;

29

FIG. 11 shows the FIG. 10 embodiment after a possible further processing step;

Fig. 12 is a diagrammatic section through another embodiment similar to Fig. 10;

Fig. 13 is a diagrammatic section through a third embodiment similar to Fig. 10;

Fig. 14 shows the Fig. FIG. 12 is a diagrammatic section through another embodiment similar to FIG. 10;

FIG. 13 is a diagrammatic section through a third embodiment similar to FIG. 10;

FIG. 14 shows the FIG. 13 embodiment after a possible further processing step; and

Fig. 15 is a diagrammatic representation of an embodiment of a sensor. FIG. 15 is a diagrammatic representation of an embodiment of a sensor.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

A first embodiment of a steering device according to the invention is shown in FIG. 1, and includes a mounting block 10, inside which there is a pressure chamber 11 containing hydraulic oil 12, the chamber 11 being nearly full of oil 12 as shown. The oil 12 is under a pressure p. Here the mounting block 10 is represented purely diagrammatically; it is substantially cylindrical here, with considerable proportions of the block extending out of Fig. 1 to the right. In FIG. 1 the mounting block 10 is represented purely diagrammatically; it is substantially cylindrical here, with considerable proportions of the block extending out of FIG. 1.

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11

The steering shaft 20 runs approximately along the cylinder axis of the mounting block 10. It thus extends through the pressure chamber 11 with the hydraulic oil 12. The shaft 20 is provided with a steering rack 21, indicated here in Fig. 1. The shaft 20 is provided with a steering rack 21, indicated here in FIG. 1 by corresponding tooth signs. The rack 21 is driven by a pinion 22. The pinion is coupled to the steering mechanism of a vehicle (not shown). When the steering wheel e.g. of a passenger car is turned the corresponding torque is transmitted through the pinion 22 to the rack 21 and displaces the whole steering shaft 20 with it along the axis through the mounting block 10.

1
2 A piston 23 is also seated on the steering shaft 20 with a non-positive
3 connection thereto. It is arranged inside the pressure chamber 11 and thus in the
4 hydraulic oil 12, whereas the pinion 22 and rack 21 are located outside the
5 chamber 11.
6
7
8

9 The steering shaft 20 thus passes through the wall of the pressure chamber
10 11 in two places. Both places are sealed by seals 24, preferably Viton seals. The
11 piston 23 moves along with the shaft 20 by virtue of its non-positive connection
12 thereto. It fills the entire cross-section of the chamber 11. The piston 23 and
13 thus the steering shaft 20 can consequently be moved by changes in the pressure
14 of the hydraulic oil 12. The piston 23, and thus the steering shaft 20, can
15 consequently be moved by changes in the pressure of the hydraulic oil 12. This
16 is a common method of strengthening the forces exerted by the user of the vehicle
17 through the pinion 22.
18
19
20

21 Suitable diameters for steering shafts 20 are about 20 to 40 mm, suitable
22 diameters for pressure chambers 11 about 40 to 70 mm, steering shafts 20 may e.g.
23 have lengths of the order of 800 mm, and the length of the pressure chamber 11
24 may e.g. be 200 to 400 mm.

25 Quite different dimensions may of course be appropriate according to the
26 requirements for the steering device, as would be known to those of skill in the art.
27

28 Quite different dimensions may of course be appropriate according to the
29 requirements for the steering device.
30

1 A mounting bore 13 is formed in the mounting block 10 outside the pressure
 2 chamber 11. It extends from the outer wall of the block 10 to the through bore in
 3 which the steering shaft 20 is located. ~~The bore 13 contains a sensor 35 which~~
 4 ~~may for example comprise the ends of a fibreglass sensory mechanism.~~

5 ~~The mounting bore 13 contains a sensor 35 which may for example comprise the~~
 6 ~~ends of a fibreglass sensory mechanism.~~

7
 8
 9 In this particular region the outside of the shaft 20 is provided with marking 30.
 10 The marking 30 comprises microstructures 31 arranged on top of the shaft 20.
 11 These are coded axially of the shaft 20 so that different bit patterns pass below the
 12 sensor 35 when the shaft 20 moves longitudinally relative to the mounting block
 13 10. ~~The signals from the sensor 35 are passed to an electronic circuit 40 (not~~
 14 ~~specifically shown in Fig. 1).~~ ~~The signals from the sensor 35 are passed to an~~
 15 ~~electronic circuit 40 (not specifically shown in FIG. 1).~~ The circuit 40 can then
 16 determine and transmit the position of the shaft 20 relative to the block 10 from
 17 the readings of the sensor 35.

18
 19
 20 Apart from the longitudinal movement of the shaft 20 other movements of the
 21 shaft are not important for the steering mechanism. ~~Hence nothing concerning any~~
 22 ~~rotation of the shaft 20 is shown in Fig. 1.~~ ~~Hence nothing concerning any rotation~~
 23 ~~of the shaft 20 is shown in FIG. 1.~~ Any versions which ensure that the pinion 22
 24 runs appropriately over the steering rack 21 are possible here.

25
 26
 27 ~~Another, alternative embodiment is shown in Fig. 2 in a view similar to~~
 28 ~~Fig. 1.~~

29 ~~Another, alternative embodiment is shown in FIG. 2 in a view similar to~~
 30 ~~FIG. 1.~~

Here again the mounting block 10 will be recognised, with the pressure chamber 11 and hydraulic oil 12.

In FIG. 2 the mounting block 10 will again be recognized, along with the pressure chamber 11 and hydraulic oil 12. The steering shaft 20 with the rack 21 again passes through the block 10 and chamber 11. Here too the pinion 22 drives the rack 21. Here too, the pinion 22 drives the rack 21. A piston 23 which can move inside the pressure chamber 11 is also seated on the shaft 20.

In contrast with Fig. 1 not only a mounting bore 13 but also a further mounting bore 14 are provided outside the pressure chamber 11.

In contrast with FIG. 1, a mounting bore 13 is not only provided, but another mounting bore 14 is also provided outside the pressure chamber 11.

This difference enables two sensors 35 and 36 to be provided. Redundant or complementary microstructures 31 of the marking 30 or microstructures double-coded in another form can therefore be read out. Redundant or complementary microstructures 31 of the marking 30 or microstructures double-coded in another form can, therefore, be read out. The sensors 35 and 36 are preferably fibre optic reflection ones. The light source for the reflection sensors is formed by light-emitting diodes (LEDs), which are spectrally adapted to the hydraulic oil 12 used in the pressure chamber 11. Pentosin may preferably be employed as the hydraulic oil 12.

The pressure p of the hydraulic oil 12 in the pressure chamber 11 is regulated by valves in a valve control housing (not shown).

1
2
3 The steering shaft 20 is sealed at the openings where it passes into and
4 out of the pressure chamber 11 by seals 24, particularly
5 Viton seals.

6 The steering shaft 20 is sealed at the openings where it passes into and out
7 of the pressure chamber 11 by seals 24, for example Viton seals. It thus has a
8 central position corresponding to the steering angle 0° . This is indicated as central
9 position X_0 in Fig. This is indicated as central position X_0 in FIG. 2. Movement
10 respectively to the right and left then takes place in the direction of steering shaft
11 position $+X$ (right) and in direction $-X$ (left). These respective end positions
12 correspond to a linear stroke which may typically be ± 75 mm. It results in
13 different stop angles of the steering mechanism according to the type of vehicle.
14 The linear stroke may also be smaller, e.g. ± 50 mm in individual cases, according
15 to the type of vehicle.

16
17
18 Here the two mounting bores 13 and 14 are arranged outside the pressure chamber
19 11, so the two individual sensors 35 and 36 are also arranged outside it.

20 In FIG. 2, the two mounting bores 13 and 14 are arranged outside the
21 pressure chamber 11, so the two individual sensors 35 and 36 are also arranged
22 outside it. It is also possible to provide an integrated pair of sensors.

23
24
25 In another embodiment the sensor or sensors 35 and 36 may be
26 positioned inside the pressure chamber 11. The sensor may then e.g. be
27 spaced from the steering shaft 20 and pick up the steering shaft data as
28 an optical sensor through the hydraulic oil 12.

In another embodiment, the sensor or sensors 35 and 36 may be positioned inside the pressure chamber 11. The sensor or sensors may then, for example, be spaced from the steering shaft 20 and pick up the steering shaft data as an optical sensor through the hydraulic oil 12.

This enables the sensor to provide information about the turbidity of the hydraulic oil 12 in the chamber 11 as well as reading the microstructures 31 of the marking 30 on the steering shaft 20.

This enables the sensor to provide information about the turbidity of the hydraulic oil 12 in the chamber 11, as well as reading the microstructures 31 of the marking 30 on the steering shaft 20. The information can be used as a criterion for changing the oil 12. A suitable transmitting wavelength for the optical sensor 35 is selected according to the turbidity and spectral absorption of the oil 12. A system of this type operates even when dirty with abraded particles or an oil film, and preferably has suitable redundancy, fault tolerance and azimuthal tolerance for safety reasons.

The sensors may be fibre optic sensors with two individual fibres, as indicated in Fig. 2 the fibres may be parallel or inclined to each other to absorb incoming and reflected light (not shown). However it is also possible to use fibre optic reflection sensors in a Y structure or to take into account arrangements with fibre lines or fibre bunches.

The sensors may be fibre optic sensors with two individual fibres. As indicated in FIG. 2, the fibres may be parallel or inclined to each other to absorb incoming and reflected light (not shown). However, it is also possible to use fibre optic reflection sensors in a Y structure or to take into account arrangements with fibre lines or fibre bunches.

1 ~~The sensors 35 and 36 or a sensor system 37 (see Fig.~~

2 ~~The sensors 35 and 36 or a sensor system 37 (see FIG. 3 for such a system)~~
 3 are employed as transmitters or receivers and may be coupled direct to the fibres
 4 by a particularly temperature-resistant installation and connection method.
 5 ~~Alternatively they may be arranged over a feed fibre located in a lower-~~
 6 ~~temperature region. In another embodiment the sensor module is fabricated as a~~
 7 ~~compact, miniaturised (microtechnical) module and mounted in the system in~~
 8 ~~order to simplify assembly.~~

9 ~~Alternatively, they may be arranged over a feed fibre located in a lower-~~
 10 ~~temperature region. In another embodiment, the sensor module is fabricated as a~~
 11 ~~compact, miniaturised (microtechnical) module and mounted in the system in~~
 12 ~~order to simplify assembly.~~

13
 14

15 In another embodiment (not illustrated) designed to increase reliability and
 16 avoid malfunctioning, two sensors 35 are juxtaposed azimuthally. These then
 17 sense two complementary bit patterns, both in the form of individual markings 30
 18 applied by the thin film method and arranged parallel, with corresponding
 19 microstructures 31.

20

21 ~~An embodiment of marking 30 with microstructures 31 is shown diagrammatically~~
 22 ~~in Fig. An embodiment of marking 30 with microstructures 31 is shown~~
 23 ~~diagrammatically in FIG. 3. Here the steering shaft 20 is reproduced purely~~
 24 ~~diagrammatically as a cut-out; it extends parallel with the x-direction indicated.~~

25

26 ~~Here, the steering shaft 20 is reproduced purely diagrammatically as a cut-out; it~~
 27 ~~extends parallel with the x-direction indicated.~~

28
 29

A sensor system 37 with an array of fibre optical Y branches 38 can further be seen. It has a module A for generating and coupling the light 51 into the input or coupling-in fibres 39 of the fibre optical Y branching element 38. It has a module "A" for generating and coupling the light 51 into the input or coupling-in fibres 39 of the fibre optical Y branching element 38.

A module B is also provided, with an array arranged in the y-direction of lenses 52, particularly microlenses, for generating parallel output beam pencils. A module "B" is also provided, with an array arranged in the y-direction of lenses 52, particularly microlenses, for generating parallel output beam pencils. The output beam pencils 53 fall onto the microstructures 31 of the marking 30 on the steering shaft 20. These microstructures 31 form a succession of sequences. Position-specific selective retroreflection takes place. The retroflected light passes back through the lenses 52 into the fibres of module B and thence to a module C for uncoupling and detecting the light 55 retroflected and leaving the fibre optical Y branching element 38.

Moreover in Fig. 3: Moreover in FIG. 3:

$\pm x$ is the axial direction, i.e. the direction of movement of the steering shaft;
 $\pm y$ is the azimuthal direction, i.e. the direction in which the position-specific bit pattern is arranged; and
 z is the direction in which the sensor system is installed.

Coordinates x and z are orthogonal to each other; coordinate z points in the direction of the tangent to the surface of the steering shaft 20 which is orthogonal to x and z.

1 ~~Fig. 4 shows a detail from Fig. 3, namely a first version of a transmitting and~~
2 ~~coupling-in module A with a single source 51, a single lens 52 and a bunch of~~
3 ~~coupling fibres 39 of the Y branching element 38.~~

4

5 ~~Fig. 5 shows an alternative to Fig. 4, a different version of a transmitting and~~
6 ~~coupling-in module A with an array of lenses 52.~~ ~~FIG. 4 shows a detail from~~
7 ~~FIG. 3, namely a first version of a transmitting and coupling-in module "A" with~~
8 ~~a single source 51, a single lens 52 and a plurality of coupling fibres 39 of the Y~~
9 ~~branching element 38.~~

FIG. 5 shows an alternative to FIG. 4, a different version of a transmitting and coupling-in module "A" with an array of lenses 52. The fibres are bunched then separated again as coupling fibres 39 of the Y branching element 38.

Fig. 6 shows another detail from Fig. 3, namely an embodiment of an uncoupling, reception and assessment module C with uncoupling fibres 54 bunched along a certain length, an array of lenses 52, a line of detectors 56, the electronic circuit 40 with the electronic assessment means and the output signal 60 with the "position of the steering shaft".

Fig. FIG. 6 shows another detail from FIG. 3, namely an embodiment of an uncoupling, reception and assessment module "C" with uncoupling fibres 54 bunched along a certain length, an array of lenses 52, a line of detectors 56, the electronic circuit 40 with the electronic assessment means and the output signal 60 with the "position of the steering shaft".

FIG. 7 shows 8-bit coding in a radial direction and periodic displacement marks in an axial direction.

Fig. FIG. 8 shows an example of an arrangement of blocks with individual coding.

Fig. 9 shows an example of an arrangement of different structure sequences and a guide structure with periodic division for tracking in the event of azimuthal displacement.

Figs 10 to 14 show embodiments of possible methods of producing the microstructures 31. FIG. 9 shows an example of an arrangement of different structure sequences and a guide structure with periodic division for tracking with azimuthal displacement.

1 FIGS. 10 - 14 show embodiments of possible methods of producing the
2 microstructures 31. A coded pattern is produced on a basic member 81, which
3 may also be the steering shaft 20 or another device non-positively coupled thereto.
4 For a version where detection is to take place by optical blanking of the patterns
5 the basic member 81 is surface-treated with a focused laser beam, so that laser-
6 ablative processes at the point of action cause stripping and thus lasting marking
7 (cf. Fig. FIG. 10).

Eximer lasers are preferably used for the purpose owing to the high resolution. The pattern thus produced can then be covered with a friction and wear-reducing film. This is shown in Fig. Eximer lasers are preferably used for this purpose, owing to their high resolution. The pattern thus produced can then be covered with a friction and wear-reducing film 82, as shown in FIG. 11. A metal-doped amorphous hydrocarbon film is eminently suitable as such a covering film in the region of the steering shaft; it is applied in a thickness of 0.5 to 5 μm by known plasma-supported PACVD processes (magnetron sputtering processes with a substrate bias and a hydrocarbon gas, preferably C_2H_2). A metal-doped amorphous hydrocarbon film is well suited as such a covering film in the region of the steering shaft, and is preferably applied in a thickness of 0.5 to 5 μm by known plasma-supported PACVD processes (magnetron sputtering processes with a substrate bias and a hydrocarbon gas, preferably C_2H_2). Titanium or tungsten is preferably employed as the doping metal for this application. The metal-doped amorphous hydrocarbon layer may for example be produced using a Leybold large capacity sputtering plant, model Tritec 1000 with two tungsten targets installed. The metal-doped amorphous hydrocarbon layer may, for example, be produced using a Leybold large capacity sputtering plant, model Tritec 1000 with two tungsten targets installed. The plant has a rotary holder which can accommodate up to 20 steering shafts according to the equipment. After the normal pumping process whereby the chamber is pumped out to about 10^{-5} hPa, argon is admitted up to a pressure of 3×10^{-3} hPa and the substrate is surface-cleaned by ion bombardment at a bias potential of 100 to 300 V. The targets are pre-sputtered at about 6 KW in the process. A graded film of tungsten-doped hydrocarbon is formed without interrupting the plasma, by opening the target covers and successively adding C_2H_2 to the process. A few minutes later the C_2H_2 gas flow is adjusted to bring the ratio of tungsten to carbon in the layer to 5 to 10%. During the production of the metal-doped amorphous hydrocarbon film the substrates are coupled with a bias potential of from 100 to 300 V, preferably 200

V. Under these conditions a film thickness of 1 μm is applied in half an hour. A few minutes later the C_2H_2 gas flow is adjusted to bring the ratio of tungsten to carbon in the layer to 5 - 10%. During the production of the metal-doped amorphous hydrocarbon film the substrates are coupled with a bias potential of from about 100 to 300 V, preferably 200 V. Under these conditions a film thickness of about 1 μm is applied in half an hour.

Other solutions explaining the use of a structured film are shown in Figs 12 to 14. The film structure may be utilised for different sensing principles. In the case of optical detection film structures may e.g. have an appropriate contrast (surface or edge contrast) with the surrounding surface. The film structure may however be produced from a magnetic material and read by means of a magnetic sensor or a magnetic sensor matrix. In that case a magnetic film is used, preferably a film of CoSm or FeSi or NdFeB with or without additives.

The steering shaft 20 or basic element 81 is coated in a vacuum process, in this case with two films 83, 84, the lower film 23 respectively being a metal-doped amorphous hydrocarbon film onto which a TiN film is deposited. Other solutions explaining the use of a structured film are shown in FIGS. 12 - 14. The film structure may be utilized for different sensing principles. In the case of optical detection, film structures may e.g. have an appropriate contrast (surface or edge contrast) with the surrounding surface. The film structure may, however, be produced from a magnetic material and read by means of a magnetic sensor or a magnetic sensor matrix. In such a case a magnetic film is used, preferably a film of CoSm or FeSi or NdFeB, with or without additives.

The steering shaft 20 or basic element 81 is coated in a vacuum process, in this case with two films 83, 84, the lower film 83 respectively being a metal-doped amorphous hydrocarbon film onto which a TiN film is deposited. The thickness of the upper film 84 is approximately 0.5 μm . TiN is preferably used in

combination with a Ti-doped hydrocarbon film. The ethine is merely substituted by nitrogen, again without interrupting the plasma. The film 84 is structured by photo-lithography, by coating the coated steering shaft 20 with a photosensitive resist. The film 84 is structured by photo-lithography, by coating the coated steering shaft 20 with a photosensitive resist. It is approximately 2.5 μm thick. The patterns are then produced over a large area on the shaft by means of a mask.

When the resist has developed the TiN film 84 is removed from places where there are no photosensitive resist patterns, by wet-chemical etching using known etching agents.

Patterns may also be made countersunk, i.e. planarised, as shown in Fig. 13. In that case the steering shaft 20 is coated e.g. with a W-doped amorphous hydrocarbon film 85, after which a photoresist pattern is formed on it. When the resist pattern has developed, the TiN film 84 is removed from places where there are no photosensitive resist patterns, by wet-chemical etching using known etching agents.

Patterns may also be made countersunk, i.e. planarized, as shown in FIG. 13. In such a case, the steering shaft 20 is coated with, for example, a W-doped amorphous hydrocarbon film 85, after which a photoresist pattern is formed on it. By means of photoresist masking a 0.2 - 1.0 μm depression is then etched in the W-doped amorphous hydrocarbon film in a reactively conducted plasma etching process (etching gases Ar/SF_6). The photoresist mask is maintained and the depression is then refilled by sputtering e.g. TiN. This makes the surface even microscopically smooth.

A further embodiment is illustrated in Fig. A further embodiment is illustrated in FIG. 14, where a tribologically optimised film 86 for the previously described substructure is applied. In this case even film materials which do not necessarily

have good tribological properties may be used to form the pattern. In this case, even film materials which do not necessarily have good tribological properties may be used to form the pattern.

An embodiment of a sensor 35 is shown in Fig. 15. This is a magnetic sensor. It comprises a linear arrangement of magnetic sensors which can read a magnetic structure e.g. in an 8-bit code. The polar structures of the reading head are shown; operating safety is improved and the number of codings increased by using a second line. The sensor 35 may for example be made from known magnetoresistive or inductive single sensors produced by similarly known thin film methods. To minimise the spacing from the magnetic microstructures on the steering shaft 20 the polar structures of the reading sensors are arranged on an arc matching the diameter of the shaft. The sensor 35 may, for example, be made from known magnetoresistive or inductive single sensors produced by similarly known thin film methods. To minimize the spacing from the magnetic microstructures on the steering shaft 20, the polar structures of the reading sensors are arranged on an arc matching the diameter of the shaft.

List of references

- 10 — mounting block
- 11 — pressure chamber
- 12 — hydraulic oil
- 13 — mounting bore
- 14 — mounting bore
- 20 — steering shaft
- 21 — steering rack

1	22	pinion
2	23	piston
3	24	seal
4		
5	30	marking
6	31	microstructures
7	35	sensor
8	36	sensor
9	37	sensor system
10	38	Y branching element
11	39	coupling fibre
12		
13	40	electronic circuit
14		
15	51	source
16	52	lens
17	53	output luminous pencil
18	54	uncoupling fibres
19	55	light
20	56	detector line
21		
22	60	output signal
23		
24	81	basic member
25	82	film
26	83	film
27	84	film
28	85	film
29	86	film
30		

- 1 A — module
- 2 B — module
- 3 C — module
- 4
- 5 p — pressure
- 6 X_0 — central position
- 7 + X — steering shaft position to the right
- 8 - X — steering shaft position to the left
- 9 y — azimuthal direction
- 10 z — direction in which sensor is installed
- 11

1 **Claims**

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It will be understood that various modifications may be made to the embodiments disclosed herein. Therefore, the above description should not be construed as limiting, but merely as exemplifications of a preferred embodiment(s). Those skilled in the art will envision other modifications within the scope and spirit of the invention.

WHAT IS CLAIMED IS:

STEERING DEVICE FOR VEHICLES

ABSTRACT

A steering device which includes coded microstructures which are provided on the steering shaft and/or on a device that is connected to the steering shaft in a non-positive manner; a sensor which detects the microstructures and outputs associated measuring signals; and an electronic circuit to which the measuring signals of the sensor are fed, and which outputs electronic signals to control the steering is disclosed.

Page 15, line 20: "~~hervorragend~~" may mean physically prominent or excellent.

Page 15, line 11: "~~Detektionsmittel~~" is probably a clerical error. "~~Detektion~~ mittels" makes more sense.

German page 15, Fig. 9: "~~in the event of~~" - alternative translation "~~with~~"

Figs 11, 14 "~~further processing step~~" - The German is actually "~~cut~~" (Schnitt), not "~~step~~" (Schritt).

Translator's Notes

1. ~~A steering device for vehicles, comprising a steering shaft (20), a sensor (35) for determining the movement of said steering shaft, and a circuit (40) for evaluating the measuring signals of the sensor (35);~~
characterised in that
coded microstructures (31) are provided on the steering shaft (20) and/or on a device that is connected to the steering shaft in a non-positive manner,

1 that a sensor (35) is provided, which detects the microstructures (31) and outputs
2 associated measuring signals, and
3 that an electronic circuit (40) is provided, to which the measuring signals of the
4 sensor (35) are fed and which outputs electronic signals for steering.

5
6 2. — A steering device according to claim 1,
7 characterised in that
8 the microstructures (31) form a succession of sequences arranged in an axial
9 direction on the steering shaft (20) and/or the device non-positively connected
10 thereto.

11
12 3. — A steering device according to claim 2,
13 characterised in that
14 each sequence comprises multiple and/or single structures arranged spatially in an
15 azimuthal and/or axial direction and containing individual or block-type coding.

16
17 4. — A steering device according to claim 2 or 3,
18 characterised in that
19 the sequences contain bit coding.

20
21 5. — A steering device according to any of claims 2 to 4,
22 characterised in that
23 a plurality of sequences are combined in a block, the blocks being distinguishable
24 from each other by coding.

25
26 6. — A steering device according to any of claims 2 to 5,
27 characterised in that

1 the sequences arranged in an axial direction are present in redundant form, offset
2 parallel more than once over the periphery of the steering shaft (20) and/or device.

3

4 ~~7. — A steering device according to any of the preceding claims,~~
5 ~~characterised in that~~
6 ~~the microstructures (31) are in complementary form.~~

7

8 ~~8. — A steering device according to any of the preceding claims,~~
9 ~~characterised in that~~
10 ~~the smallest details of the microstructures (31) have lateral dimensions of 5 nm to~~
11 ~~5 mm.~~

12

13 ~~9. — A steering device according to claim 8,~~
14 ~~characterised in that~~
15 ~~the smallest details of the microstructures (31) have lateral dimensions of 1 µm to~~
16 ~~1 mm.~~

17

18 ~~10. — A steering device according to any of the preceding claims,~~
19 ~~characterised in that~~
20 ~~the microstructures (31) have a thickness of 5 nm to 1 mm.~~

21

22 ~~11. — A steering device according to claim 10,~~
23 ~~characterised in that~~
24 ~~the microstructures (31) have a thickness of 100 nm to 100 µm.~~

25

26 ~~12. — A steering device according to any of the preceding claims,~~
27 ~~characterised in that~~

1 ~~the microstructures (31) have a level surface and are levelled by a planarising~~
2 ~~method.~~

3
4 ~~13. — A steering device according to any of the preceding claims,~~
5 ~~characterised in that~~
6 ~~the microstructures are built up from or covered with tribological hard-material~~
7 ~~layered systems.~~

8
9 ~~14. — A steering device according to claim 13,~~
10 ~~characterised in that~~
11 ~~the hard-material layered systems are single films or multi-layer films of TiN~~
12 ~~and/or TiAlN and/or TiCN films and/or aluminium oxide films and/or amorphous~~
13 ~~diamantine hydrocarbon films with and without metal doping and/or amorphous~~
14 ~~CN films and/or cubic boron nitride films and/or diamond films.~~

15
16 ~~15. — A steering device according to any of the preceding claims,~~
17 ~~characterised in that~~
18 ~~the sensors (35) are arranged in the form of a line and/or array.~~

19
20 ~~16. — A steering device according to any of the preceding claims,~~
21 ~~characterised in that~~
22 ~~the sensors (35) are optical sensors.~~

23
24 ~~17. — A steering device according to claim 16,~~
25 ~~characterised in that~~
26 ~~the sensors (35) are optical fibreglass sensors.~~

27
28 ~~18. — A steering device according to claim 17~~

- 1 characterised in that
2 the sensors (35) are fibre-optical double or multiple sensors.
3
- 4 19. — A steering device according to any of claims 16 to 18,
5 characterised in that
6 the microstructures are in the form of a reflection hologram.
7
- 8 20. — A steering device according to any of claims 1 to 15,
9 characterised in that
10 the sensors (35) are magnetic sensors.
11
- 12 21. — A steering device according to claim 20;
13 characterised in that
14 the magnetic sensors are in a linear arrangement for reading a multi-bit code,
15 particularly an 8-bit code.
16
- 17 22. — A steering device according to claim 20 or 21,
18 characterised in that
19 the sensor (35) has a reading head with polar structures arranged on an arc
20 matching the diameter of the steering shaft (20).
21
- 22 23. — A method of making a steering device according to any of the preceding
23 claims,
24 characterised in that
25 the microstructures on the steering shaft (20) or on the device non-positively
26 connected to the shaft are produced using thin film methods, and that structuring
27 is effected by photo-lithographic methods.
28

1 ~~24. — A method according to claim 23,~~
2 ~~characterised in that~~
3 ~~the thin-film method is a PVD and/or CVD method.~~

4
5 ~~25. — A method according to claim 23 or 24,~~
6 ~~characterised in that~~
7 ~~the microstructures are formed by a dry etching process and/or a wet-chemical~~
8 ~~etching process.~~

9
10 ~~26. — A method of making a steering device according to any of claims 1 to 22,~~
11 ~~characterised in that~~
12 ~~the microstructures are produced by a laser beam process.~~

13
14 ~~27. — A method according to claim 26,~~
15 ~~characterised in that~~
16 ~~the laser beam process used is a direct-writing laser ablation process and/or a~~
17 ~~laser-lithographic process and/or a direct-action mask-related laser-structuring~~
18 ~~process.~~

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